بررسی مشخصات خودسوییچ ماختندری مبتنی بر تقویت کننده نوری نیمرسانا

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چکیده
در این مقاله مکانیزم خودسوییچ ماختندری مبتنی بر تقویت کننده نوری نیمرسانا (SOA) با استفاده از پاسخ دینامیک برهنگی SOA مورد بررسی قرار گرفته است. پارامترهای کلیدی ساختاری و پالس ورودی خودسوییچ تعیین و تأثیر آنها بر عملکرد خودسیج بررسی شده است. برای تعیین پاسخ دینامیک برهنگی SOA، باید پارامترهای خودسیج تعیین و انتخاب شوند. نتایج شبیه‌سازی نشان می‌دهند که برای بهترین عملکرد خودسیج، پارامترهای مربوط به خودسیج نیاز به تغییر و تغییرات پارامترهای کلیدی در خودسیج مورد نظر است.

کلید واژه‌ها: ماختندری، تغییرات پارامترهای کلیدی، خودسیج تمام نوری

Investigation of SOA-Based MZI Self-Switch Characteristics

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Abstract- In this paper, we present self-switching mechanism using Semiconductor Optical Amplifier (SOA)-assisted Mach-Zehnder interferometer (MZI) considering dynamic gain response of the SOA. The effect of key structural and input pulse parameters of an all-optical MZI self-switches is identified and their role in the operation of self-switch is analyzed. The optimum values of these parameters must be correctly selected and adapted so as to ensure the satisfaction of the best operating conditions. Simulation results demonstrate that key parameters must be suitably modified to the specific all-optical self-switching application.

Keywords: Mach-Zehnder interferometer, performance parameters variation, Semiconductor Optical Amplifier, All-optical self-switch.

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1 Introduction

Semiconductor optical amplifier (SOA) is a promising element in All-optical communication networks. The switching attractive features of SOA are the fast switching time, low power consumption, high repetition rate, compactness, and high non-linear properties [1]. These features caused to SOA-assisted Mach-Zehnder interferometer (MZI) all-optical switches have been of large attention in research. These switches will perform a set of critical network processing functions such as shift register with inverter, address recognition, full adder and multi/demultiplexing [2].

Self-switching (or asymmetric switching) is a technique that input signal can be switched to desire output port where the input signal is split unequally over the MZI arms without using high power extra switching signals. SOA–MZI self-switch has been used to perform various tasks such as pulse shaping [3], pattern effect compensator, all-optical time-domain label recognition, and low-loss optical combiner.

By using rate equation model (REM) we can describe the nonlinear gain and phase dynamics of SOA in a phenomenological way. The cross-phase modulation (XPM) and self-phase modulation (SPM) are common techniques to extract the SOA nonlinearities as switching nonlinear element [4]. Because of the unequally splitting input signal over the interferometer arms, two SOAs are operating in different gain regimes, obtaining a phase difference between the two signals which are propagated in each arm. Besides, due to the finite experiences a different phase shift relative to the lagging edge. SPM will change the pulse shape as well as its spectrum [5].

We propose here the effect of structural and input pulse parameters which have not been considered altogether comprehensively in previous MZI self-switches is considered.

2 Principle of Operation

The schematic diagram of the SOA-assisted MZI self-switch is shown in figure 1. When an input pulse launched at the input port 1, is split asymmetrically to each arm by the coupler. In the high optical power arm, the SOA experiences SPM, causing changes of both the gain and the refractive index as a function of entrance intensity. The phase shift of one of the SOA’s is changed with respect to the other one by $\Delta \phi$. As a result, due to SOA nonlinearities the phase difference occurs between these two pulses. If the phase difference between these pulses reaches adequate amount ($\pi$) the input pulse in Port 1 will be switched to switching port (Port 3 in figure 1) [5].

3 Model Formulation

The optical input pulse injected in the input port 1, is distributed unequally as SOA1 and SOA2 input pulses. The power splitting ratios in input and output coupler are X and Y-1 respectively. The SOA1 and SOA2 input pulse powers after passing through input coupler are $X \times P_{in}$ and $(1-X) \times P_{in}$ respectively, where $P_{in}$ is input pulse power. As mentioned before, SOA induces a nonlinear phase shift ($\Delta \phi$) to these optical pulses. When $\Delta \phi = \pi$, maximum extinction ratio between switch outputs (Port 3 and Port 4) can be reached. The switching window of the proposed port (port 3) can be expressed as [5]

$$SW(t) = XYG_1(t) + (1-X)(1-Y)G_2(t) - 2\sqrt{XY(1-X)(1-Y)G_1(t)G_2(t)\cos(\Delta \phi)}$$  \hspace{1cm} (1)

The basic interferometric equations that describe the self-switch output (port 3 and port 4), can be written as [6]

$$P_3(t) = \frac{P_{in}}{2}\left[XYG_1(t) + (1-X)(1-Y)G_2(t) - 2\sqrt{XY(1-X)(1-Y)G_1(t)G_2(t)\cos(\Delta \phi)}\right]$$  \hspace{1cm} (2)

$$P_4(t) = \frac{P_{in}}{2}\left[X(1-Y)G_1(t) + (1-X)YG_2(t) + 2\sqrt{XY(1-X)(1-Y)G_1(t)G_2(t)\cos(\Delta \phi)}\right]$$  \hspace{1cm} (3)

respectively. Where $G_1(t)$ and $G_2(t)$ are the SOA1 and SOA2 gain seen by the data pulses. These two parameters are related to $\Delta \phi$ by [1]

$$\Delta \phi = -\frac{\alpha_n}{2} \ln\left(\frac{G_1(t)}{G_2(t)}\right)$$  \hspace{1cm} (4)

3.1 SOA Modelling

To take into account the electrical fields propagation in the SOA for picosecond regime, a
theoretical basic model is solved numerically. The electrical fields is written as [4]

$$E(z,t) = A(z,t)\exp[-i(\omega_0 t + \mu \beta_0 z)]$$  \hspace{1cm} (5)

Here, $A$ is slowly varying complex envelope function of a propagating optical pulse in the SOA length; $\omega_0/2\pi$ is carrier frequency, and $\beta_0$ is propagating constant in SOA at transparency. The envelop propagation is described by the well-known equation [6]

$$\frac{\partial A}{\partial z} + v_g \frac{\partial A}{\partial t} = g(1-i\alpha_N)A$$ \hspace{1cm} (6)

Where, $v_g$ is group velocity, $\alpha_N$ is line width enhancement factor associated with the gain change due to carrier depletion. Due to relatively narrow spectral width of optical pulse, the field gain $g$ is assumed to be frequency independent. Otherwise, $g$ in Eq. (6) should be replaced by an operator including second order time derivative [7]. The interaction between pulses and SOA is described by the (7) ordinary differential rate equation [6]. Where $\tau$ is carrier lifetime, $E_{sat}$ is saturation energy of SOA. The small-signal gain coefficient per unit SOA length (linear gain) $g_0$ is determined by current injection.

$$\frac{\partial g}{\partial t} = \frac{g_0 - g}{\tau} - \frac{g |A|^2}{E_{sat}}$$ \hspace{1cm} (7)

### 4 Results and Discussions

The critical role of the SOA in the operation of the self-switch caused to investigate and understand the SOA dynamical behaviour with respect to several key operational parameters, such as the input pulse energy, input and output couplers unequal power splitting, and the SOA unsaturated power gain. We set the parameters as mentioned [4].

Figure 2 shows the normalized output power ($P_3/P_{3,\text{max}}$) and extinction ratio ($P_3/P_4$), by replacing $P_3$ and $P_4$ from (2) and (3), versus input pulse energy ($E_{in}$). For the normalized output power, increasing $E_{in}$ enhances the depletion of carriers, so that the data pulses experiences a higher gains. Increasing SOA1 and SOA2 gains cased to the normalized output power increasing. The larger is $E_{in}$, the deeper is the SOA2 saturation and the steeper gain transition from the initial small signal to the final saturation value. On the other hand, as mentioned in Eq. (4), the gain ratio ($G_1/G_2$) for the pulses must be reaches adequate amount to have reaches desired phase difference ($\pi$). The result reveals that to have switching operation the input pulse energy should be 0.65 pJ < $E_{in}$ < 2.85 pJ. For $E_{in}$ = 1.3 pJ the phase difference between two data pulses reaches $\pi$ and biggest extinction ration is achieved.

Figure 3 depicts the influence of the input and output couplers unequal power splitting on the switching characteristics. At $X=Y=0.5$ two data pulses have equal power pulses and hence equal gains ($G_1=G_2$). Therefore according to Eq. (4), $\Delta \phi$ is equivalent to a zero and the full destructive interference at the Port 3 will occurred. By increasing amount of $X(Y)$, the gain ratio of pulses and $\Delta \phi$ increases. For $X = Y = 1$, the full constructive interference at the Port 3 will be occurred which in turn leads to the phase difference between two data pulses reaches $\pi$ and hence biggest extinction ration is achieved. As shown in figure 3 for $X(Y)< 0.125$ and $X(Y)> 0.875$, the gain ratio of input pulses will be increased which in turn leads to input signal can be switched to desire output (port 3).

Figure 4 illustrates the unsaturated power gain ($G_0$) effect. An increased $G_0$ results in a gain variation
far away from heavy saturation that cause to the
 gain seen by the pulses increases. The result shows
 that to have switching operation the unsaturated
 power gain should be $18 \, \text{dB} < G_0 < 24 \, \text{dB}$. For $G_0 =
 21 \, \text{dB}$ the phase difference between two data
 pulses reaches $\pi$ and biggest extinction ration
 is achieved.

Figure 5 shows the input pulse is transmitted to
 port 3 (switching port) and the switching
 function will be achieved. Measured in FWHM, SOA1,
 SOA2, and port 3 output pulses are slightly expanded
 with an asymmetry shortening their leading edges, as is usually observed with SOA.
 These expansion and asymmetry shortening are
 more significant for port 3 output pulse.

**Figure 4**: Normalized output power and extinction ratio
 from switching port 3, versus unsaturated power gain

**Figure 5**: Calculated SOA’s and self-switch output
 pulses temporal profile

### 5 Conclusion

We numerically analysed self-switching
 mechanism in SOA-based MZI interferometer by
 unequal distribution of input optical pulse. We
 showed that the switching characteristics can be
 accomplished by varying the input pulse energy,
couplers unequal power splitting coefficient, and
 SOA’s unsaturated gain.

**References**

[1] M. J. Connelly, Semiconductor Optical

 interferometer-based high-speed OTDM add-

 and self-routing in a 250Gbit/s packet-

 properties of contra-propagating picosecond
 optical pulses in SOA,” *Optics Communications*, Vol. 259, No. 2, pp. 465–
 469, 2006.

 Fredkin gate,” *IEEE J. Sel. Top. Quantum

 modulation and spectral broadening of optical
 pulses in semiconductor laser amplifiers,”
 *IEEE journal of quantum electronics*, Vol. 25,
 No. 11, pp. 2297-2306, 1989.

[7] M. Razaghi, V. Ahmadi, M. J. Connelly,
 “Comprehensive finite-difference time
 dependent beam propagation model of
counter propagation picosecond pulses in a
semiconductor optical amplifier,” *J.